

Distributed Two-Way Localization Bounds for 5G mmWave Systems

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Abstract—Recently, localization for 5G millimeter-wave communication systems has been shown to provide high-accuracy performance, with error being in the order of tens of centimeters. However, most of the literature assumes a high level of synchronization, which is not always the case practically. To address this matter, we investigate a distributed two-way localization protocol (DLP) that relieves the need for tight timing synchronization. We derive the position and orientation bounds, when localization is initiated and carried out by the base station. Our simulation results show that the performance of DLP is identical to that of the synchronized one-way localization. We thus conclude that the considered 5G localization is limited by the estimation of the angles rather than the delay. The results also imply that orientation estimation is more challenging than position estimation.

I. INTRODUCTION

With the high localization accuracy of 5G millimeter-wave (mmWave) communication systems, location-aided communication is becoming more attractive. The location information creates two kinds of opportunities unique to 5G mmWave, since it enables location-aware applications [1], [2], e.g., vehicular communication, and assisted living systems, while also supporting communication systems design and optimization [3]–[5] such as beamforming, pilot assignment, and resources allocation.

Due to the utilization of arrays with high number of antennas at the transmitter and the receiver, and the allocation of massive bandwidths, spatiotemporal localization with single base station (BS) can be seen as the ultimate localization strategy for 5G. With the high number of antennas, the directions of arrival (DOA) and departure (DOD) can be estimated with very low error [6], while the large bandwidth enables highly accurate estimation of the time of arrival (TOA) [7]. Subsequently, combining the spatial and temporal estimates, the user equipment (UE) location can be determined.

The accuracy of single-anchor localization for 5G mmWave systems has been studied recently by several papers in terms of position (PEB) and orientation error bounds (OEB). The UE PEB and OEB of 2D localization in 5G mmWave systems were investigated in [8] using uniform linear arrays. On the other hand, the PEB and OEB for mmWave 3D localization were derived with different approaches in [9] and [10] using arrays with arbitrary geometries. The results in [8]–[10] showed that the error performance of 5G mmWave localization is in the order of centimeters. However, one important, yet usually

overlooked, requirement for localization is the synchronization of BS and UE. For example, [8] and [10] assume that the BS and UE are perfectly synchronized, while [9] assumes coarse synchronization, and includes a residual synchronization error in the model.

Motivated by two-way ranging that uses the time-of-flight [11], in this paper, we focus on two-way localization (TWL). We study the PEB and OEB under line-of-sight (LOS) communication with a distributed TWL protocol (DLP) that accounts for timing bias between the clocks of the BS and UE. Higher order artifacts such as clock drift and skew are not addressed herein, but can be estimated using three- or multi-way ranging [11], [12]. Under DLP, the BS initiates the localization process by transmitting a known signal to a UE. Then, the UE estimates the TOA with reference to its local clock and transmits back another known signal, after a pre-agreed waiting interval. Subsequently, upon receiving the UE signal, the BS estimates the range between the two devices with reference to its local clock. Since this clock was initially used to transmit the first signal, full time synchronization between UE and BS is not needed. Eventually, localization is achieved at the BS, using the signal received back after the second transmission round.

Considering localization at BS only, we investigate the DLP for LOS 5G mmWave signals, as a means of alleviating the tight synchronization requirement of localization. Towards that, we consider the timing bias between the BS and UE as a nuisance parameter and derive the Fisher information matrices (FIM) of the position and orientation. Based on these FIMs, we evaluate the PEB and OEB numerically, and compare them to those of the traditional one-way localization (OWL) [10]. The results provided herein are part of an extensive study presented in [13], where both network-side and device-side localization are investigated for distributed and centralized TWL protocols.

II. CHANNEL MODEL AND BEAMFORMING

Consider uplink localization, whereby a BS, located at the origin of the 3D space with zero orientation angles, attempts to estimate the UE position, $\mathbf{p} \triangleq [p_x, p_y, p_z]^T$, and orientation, $\mathbf{o} \triangleq [\zeta_0, \chi_0]^T$. Similar to [10], we define ζ_0 as the rotation angle around the z -axis, which yields new coordinate axes x' , y' and z , while χ_0 is defined as the rotation angle around the x' -axis. See Fig. 1. This is representative of practical applications characterized by two rotation angles, such as vehicular and robotic

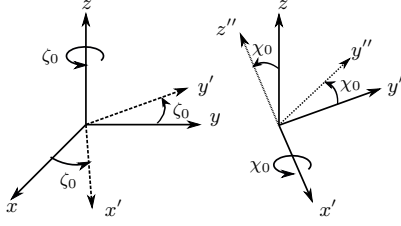


Fig. 1. Two-step rotation: First around z -axis, then around x' -axis.

applications¹. Both BS and UE are equipped with antenna arrays of arbitrary but known geometries and communicate through a LOS. In this context, we assume that the NLOS parameters, if any, can be estimated as in [10]. However, unlike [10], we use only the DOA, DOD and TOA of the LOS path to compute the PEB and OEB. Consequently, for clarity, we can write the signal model explicitly by including only the LOS².

In the following, the parameters related to BS and UE are denoted by the subscripts “B” and “U”, respectively, while the superscripts “f” and “b” denote the parameters to the forward and backward transmissions, respectively.

1) *Forward Channel*: The *forward* signal, received at UE at time $t = \tau^f$, undergoes a channel given by

$$\mathbf{H}^f(\beta, \boldsymbol{\vartheta}) \triangleq \mathbf{H}_s^f(\beta, \boldsymbol{\vartheta})\delta(t - \tau^f), \in \mathbb{C}^{N_U \times N_B} \quad (1)$$

where $\mathbf{H}_s^f(\beta, \boldsymbol{\vartheta}) \triangleq \sqrt{N_B N_U} \beta \mathbf{a}_U(\theta_U, \phi_U) \mathbf{a}_B^H(\theta_B, \phi_B)$ is the channel part corresponding to the spatial channel parameters, such that β is the complex path gain, N_B and N_U are the number of antennas at BS and UE, respectively, and

$$\boldsymbol{\vartheta} \triangleq [\theta_B, \phi_B, \theta_U, \phi_U]^T, \quad (2)$$

and (θ_U, ϕ_U) and (θ_B, ϕ_B) are the forward DOAs and DODs. Finally, \mathbf{a}_U and \mathbf{a}_B are the array response vectors

$$\mathbf{a}_U(\theta_U, \phi_U) \triangleq \frac{1}{\sqrt{N_U}} e^{-j\boldsymbol{\Delta}_U^T \mathbf{k}(\theta_U, \phi_U)}, \quad \in \mathbb{C}^{N_U} \quad (3)$$

$$\mathbf{a}_B(\theta_B, \phi_B) \triangleq \frac{1}{\sqrt{N_B}} e^{-j\boldsymbol{\Delta}_B^T \mathbf{k}(\theta_B, \phi_B)}, \quad \in \mathbb{C}^{N_B} \quad (4)$$

where $\mathbf{k}(\theta, \phi) = \frac{2\pi}{\lambda} [\cos \phi \sin \theta, \sin \phi \sin \theta, \cos \theta]^T$ is the wavenumber vector, λ is the wavelength, $\boldsymbol{\Delta}_B \in \mathbb{C}^{3 \times N_B}$ is a matrix whose columns contain the 3D Cartesian coordinates of the array elements of BS in meters, and $\boldsymbol{\Delta}_U \in \mathbb{C}^{3 \times N_U}$ is defined similarly for UE. For presentation purposes, we drop the angle parameters from the notation of \mathbf{a}_B and \mathbf{a}_U .

The signal transmitted from BS is modeled by $\sqrt{E_t} \mathbf{F}_B \mathbf{s}_B(t)$, where E_t is the transmitted energy per symbol, and $\mathbf{F}_B \triangleq [\mathbf{f}_{B,1}, \mathbf{f}_{B,2}, \dots, \mathbf{f}_{B,N_{bB}}]$ is the BS transmit beamforming matrix, $\mathbf{f}_{B,b}, 1 \leq b \leq N_{bB}$ is the b^{th} BS beam, and N_{bB} is the number of transmit beams. The pilot signal $\mathbf{s}_B(t) \triangleq$

¹This corresponds for instance to a vehicle that can turn left and right (ζ_0) or ascend and descend (χ_0), but does not slip or flip.

²The protocols presented in this paper could also exploit the reflected components for positioning. Conceptually, this can be done by applying the path orthogonality arguments presented in [10].

$[\mathbf{s}_{B,1}(t), \mathbf{s}_{B,2}(t), \dots, \mathbf{s}_{B,N_{bB}}(t)]^T$ has

$$\mathbf{s}_{B,b}(t) = \sum_{\ell=0}^{N_s-1} a_{B,\ell}^{(b)} p(t - \ell T_s), \quad 1 \leq b \leq N_{bB}, \quad (5)$$

where $a_{B,\ell}^{(b)}$ are known unit-energy pilot symbols transmitted over the b^{th} beam from BS, and $p(t)$ is a unit-energy pulse with a power spectral density (PSD), denoted by $|P(f)|^2$. In (5), N_s is the number of pilot symbols and T_s is the symbol duration, leading to a total observation time of $T_o \approx N_s T_s$. Note that we keep the transmitted power fixed with N_{bB} by setting $\text{Tr}(\mathbf{F}_B^H \mathbf{F}_B) = 1$, and $\mathbf{s}_B(t) \mathbf{s}_B^H(t) = \mathbf{I}_{N_{bB}}$, where $\text{Tr}(\cdot)$ denotes the matrix trace, and $\mathbf{I}_{N_{bB}}$ is the identity matrix.

Similarly, define the receive beamforming matrix at UE as $\mathbf{W}_U \triangleq [\mathbf{w}_{U,1}, \mathbf{w}_{U,2}, \dots, \mathbf{w}_{U,N_{bU}}]$, where $\mathbf{w}_{U,k}, 1 \leq k \leq N_{bU}$ is a UE receive beam, and N_{bU} is the number of receive beams.

2) *Backward Channel*: Channel from UE to BS is

$$\mathbf{H}^b(\beta, \boldsymbol{\vartheta}) \triangleq \mathbf{H}_s^b(\beta, \boldsymbol{\vartheta})\delta(t - \tau^b) \in \mathbb{C}^{N_B \times N_U}, \quad (6)$$

where $\mathbf{H}_s^b(\beta, \boldsymbol{\vartheta}) \triangleq \sqrt{N_B N_U} \beta \mathbf{a}_B(\theta_B, \phi_B) \mathbf{a}_U^H(\theta_U, \phi_U)$, such that τ^b denotes the local TOA at BS, (θ_U, ϕ_U) and (θ_B, ϕ_B) are the backward DODs and DOAs at UE and BS, respectively. We assume that both transmissions occur within the coherence time so that the channel gain remains unchanged. In the backward transmission, UE transmits with a beamforming matrix, \mathbf{F}_U containing N_{bU} beams, while BS receives via a beamforming matrix, \mathbf{W}_B containing N_{bB} beams. Both \mathbf{F}_U and \mathbf{W}_B are defined similar to \mathbf{W}_U and \mathbf{F}_B , respectively, but with possibly different beam directions.

Our objective is to derive the error bounds of estimating \mathbf{p} and \mathbf{o} , from TOA, DOA, and DOD, obtained through DLP, in the presence of timing offset, B , and path gain, β , as nuisance parameters.

III. DISTRIBUTED TWO-WAY LOCALIZATION PROTOCOL

In our formulation, we assume that the UE has a *clock bias* with respect to the BS clock, denoted by B . We denote the propagation delay (nominal TOA) by $\tau = \|\mathbf{p}\|/c$, where c is the speed of light. See Fig. 2.

The forward transmission is initiated by the BS at time $t = 0$, and received at UE at local time

$$t = \tau^f = B + \tau. \quad (7)$$

Consequently, the observed signal after beamforming at the UE is given by

$$\mathbf{y}_U(t) = \sqrt{E_t} \mathbf{W}_U^H \mathbf{H}_s^f(\beta, \boldsymbol{\vartheta}) \mathbf{F}_B \mathbf{s}_B(t - \tau^f) + \mathbf{n}_U(t), \quad (8)$$

Denoting the real and imaginary parts of β by β_R and β_I , we find the FIM of $[\boldsymbol{\vartheta}^T, \beta_R, \beta_I, \tau^f]^T$ based on $\mathbf{y}_U(t)$.

On the other hand, the backward transmission is initiated by the UE at time $t = t^b$, and received by BS at a local time

$$t = \tau^b = t^b + \tau - B. \quad (9)$$

After a pre-agreed delay τ^D , measured from the time $\mathbf{y}_U(t)$ is received, UE sends back a signal $\mathbf{s}_U(t)$ at

$$t^b = \hat{\tau}^f + \tau^D.$$

Subsequently, BS receives the signal $\mathbf{y}_B(t)$ at

$$\tau^b = \hat{\tau}^f + \tau^D + \tau - B = 2\tau + e^f + \tau^D. \quad (10)$$

Thus, the observed signal after beamforming at BS is

$$\mathbf{y}_B(t) = \sqrt{E_t} \mathbf{W}_B^H \mathbf{H}_s^b(\beta, \boldsymbol{\vartheta}) \mathbf{F}_U \mathbf{s}_U(t - \tau^b) + \mathbf{n}_B(t) \quad (11)$$

Based on $\mathbf{y}_B(t)$, BS estimates $\hat{\tau}^b$ and eventually determines \mathbf{p} , and \mathbf{o} . Note that B in the forward and backward transmissions cancel out, and need not be estimated at UE. Thus, based on $\mathbf{y}_B(t)$, the FIM of $[\boldsymbol{\vartheta}^T, \beta_R, \beta_I, \tau^b]^T$ is determined.

Denoting the equivalent FIMs (EFIMs) of τ^f and τ^b by J_{τ^f} and J_{τ^b} , respectively, we introduce the following estimation error notation

$$e^f \triangleq \hat{\tau}^f - \tau^f, \quad \text{and} \quad e^b \triangleq \hat{\tau}^b - \tau^b, \quad (12)$$

such that

$$\mathbb{E}\{(e^f)^2\} \geq J_{\tau^f}^{-1}, \quad \mathbb{E}\{(e^b)^2\} \geq J_{\tau^b}^{-1}. \quad (13)$$

Finally, since the received signals are observed at the beamformer output, the noise terms in (8) and (11) are zero-mean additive *spatially-correlated* Gaussian noise. Therefore, the corresponding noise auto-covariance matrices are $\mathbf{R}_{\mathbf{n}_U} = N_0 \mathbf{W}_U^H \mathbf{W}_U$, and $\mathbf{R}_{\mathbf{n}_B} = N_0 \mathbf{W}_B^H \mathbf{W}_B$ where N_0 is the noise PSD, which is assumed to be identical at BS and UE.

IV. DERIVATION OF PEB AND OEB FOR DLP

The PEB and OEB can be computed from the EFIM of position and orientation, $\mathbf{J}_{\mathbf{o}, \mathbf{p}}^e$,

$$\text{OEB} \triangleq \sqrt{[\mathbf{J}_{\mathbf{o}, \mathbf{p}}^e]_{1,1} + [\mathbf{J}_{\mathbf{o}, \mathbf{p}}^e]_{2,2}}, \quad (14)$$

$$\text{PEB} \triangleq \sqrt{[\mathbf{J}_{\mathbf{o}, \mathbf{p}}^e]_{3,3} + [\mathbf{J}_{\mathbf{o}, \mathbf{p}}^e]_{4,4} + [\mathbf{J}_{\mathbf{o}, \mathbf{p}}^e]_{5,5}}. \quad (15)$$

Since $\mathbf{J}_{\mathbf{o}, \mathbf{p}}^e$ is obtained by transforming the FIM of channel parameters, we start by computing this FIM. Then, we derive PEB and OEB using a parameter transformation procedure similar to [10].

1) *FIM of Channel Parameters*: In light of (6), (10) and (11), the vector of the unknowns under DLP is defined by

$$\boldsymbol{\varphi}_D \triangleq [\boldsymbol{\vartheta}^T, \beta_R, \beta_I, \tau]^T. \quad (16)$$

Consequently, the FIM of $\boldsymbol{\varphi}_D$ is defined as

$$\mathbf{J}_{\boldsymbol{\varphi}_D} \triangleq \begin{bmatrix} \mathbf{J}_{\boldsymbol{\vartheta}\boldsymbol{\vartheta}}^b & \mathbf{0}_6 \\ \mathbf{0}_6^T & J_{\tau\tau} \end{bmatrix}, \quad (17)$$

where,

$$\mathbf{J}_{\boldsymbol{\vartheta}\boldsymbol{\vartheta}}^b = \begin{bmatrix} \mathbf{J}_{\boldsymbol{\vartheta}\boldsymbol{\vartheta}}^b & \mathbf{J}_{\boldsymbol{\vartheta}\beta}^b \\ \left(\mathbf{J}_{\boldsymbol{\vartheta}\beta}^b\right)^T & J_{\beta_R \beta_R}^b \mathbf{I}_2 \end{bmatrix}, \quad (18)$$

is the FIM corresponding to the spatial part of $\mathbf{J}_{\boldsymbol{\varphi}_D}$. The value of $J_{\tau\tau}$ as well as the entries of (18) are derived in the Appendix. Note that, as discussed in [10], the temporal and spatial parts in (17) are independent based on realistic mmWave assumptions: large number of transmit and receive antennas, large bandwidth and spatially sparse channel. Moreover, note that in (18), we used the fact that $J_{\beta_R \beta_R}^b = J_{\beta_I \beta_I}^b$.

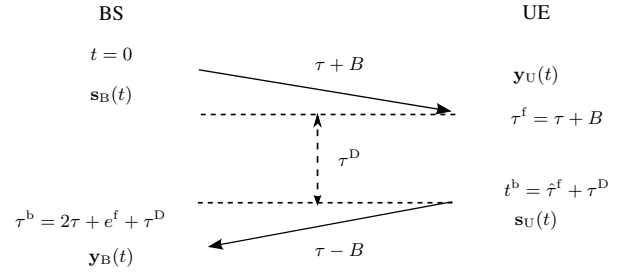


Fig. 2. The timeline of the distributed TWL protocol.

While we can determine J_{τ^f} based on $\mathbf{y}_U(t)$, the FIM of $[\boldsymbol{\vartheta}^T, \beta_R, \beta_I, \tau^b]^T$ is based on $\mathbf{y}_B(t)$. Hence, to obtain the FIM of $\boldsymbol{\varphi}_D$ that includes τ rather than τ^b , we apply the fact that the delays are independent of any other parameter [10]. Towards that, recall that $\hat{\tau}^b = 2\tau + e^f + e^b + \tau^D$, and define

$$\tau' \triangleq \frac{\hat{\tau}^b - \tau^D}{2} = \tau + \frac{e^f + e^b}{2}. \quad (19)$$

Consequently, using (13) yields

$$\mathbb{E}\{(\tau' - \tau)^2\} \geq \frac{1}{4} (J_{\tau^f}^{-1} + J_{\tau^b}^{-1}), \quad (20)$$

that is,

$$J_{\tau\tau} = 4 (J_{\tau^f}^{-1} + J_{\tau^b}^{-1})^{-1}. \quad (21)$$

2) *FIM of Location Parameters*: To obtain the FIM of the location parameters (position and orientation), we need the EFIM of $\boldsymbol{\vartheta}$ and τ . Since the temporal and spatial parts in (17) are independent, the EFIM of DOD and DOA is obtained from (18) by Schur's complement

$$\mathbf{J}_{\boldsymbol{\vartheta}\boldsymbol{\vartheta}}^{e,b} = \mathbf{J}_{\boldsymbol{\vartheta}\boldsymbol{\vartheta}}^b - \frac{1}{J_{\beta_R \beta_R}^b} \mathbf{J}_{\boldsymbol{\vartheta}\beta}^b \left(\mathbf{J}_{\beta\beta}^b\right)^T. \quad (22)$$

Consequently, the EFIM of $\boldsymbol{\vartheta}$ and τ is given by

$$\mathbf{J}_{\boldsymbol{\vartheta}\tau}^{e,b} = \begin{bmatrix} \mathbf{J}_{\boldsymbol{\vartheta}\boldsymbol{\vartheta}}^{e,b} & \mathbf{0}_4 \\ \mathbf{0}_4^T & J_{\tau\tau} \end{bmatrix}. \quad (23)$$

Applying a parameter transformation to (23), we obtain the EFIM of orientation and position

$$\mathbf{J}_{\mathbf{o}, \mathbf{p}}^{e,b} = \boldsymbol{\Upsilon} \mathbf{J}_{\boldsymbol{\vartheta}\tau}^{e,b} \boldsymbol{\Upsilon}^T, \quad (24)$$

where $\boldsymbol{\Upsilon} \triangleq [\boldsymbol{\Upsilon}_s \ ; \ \boldsymbol{\Upsilon}_\tau]$ is UL transformation matrix,

$$\boldsymbol{\Upsilon} \triangleq \begin{bmatrix} \frac{\partial \theta_B}{\partial \boldsymbol{\vartheta}} & \frac{\partial \phi_B}{\partial \boldsymbol{\vartheta}} & \frac{\partial \theta_U}{\partial \boldsymbol{\vartheta}} & \frac{\partial \phi_U}{\partial \boldsymbol{\vartheta}} & \vdots & \frac{\partial \tau}{\partial \boldsymbol{\vartheta}} \\ \frac{\partial \theta_B}{\partial \mathbf{p}} & \frac{\partial \phi_B}{\partial \mathbf{p}} & \frac{\partial \theta_U}{\partial \mathbf{p}} & \frac{\partial \phi_U}{\partial \mathbf{p}} & \vdots & \frac{\partial \tau}{\partial \mathbf{p}} \end{bmatrix},$$

such that [10]

$$\boldsymbol{\Upsilon}_s = \begin{bmatrix} 0 & 0 & -\frac{p'_y}{a'} & -\frac{p'_x p'_z}{a'^2} \\ 0 & 0 & \frac{p'_x \sin \chi_0}{a'} & -\frac{p'_x \cos \chi_0 + g p'_y}{a'^2} \\ \frac{\dot{\mathbf{p}}_\theta}{\|\dot{\mathbf{p}}\| a} & \frac{[-p_y, p_x, 0]^T}{a^2} & \mathbf{r}_3 + \frac{p'_z}{a'} \mathbf{P} & \frac{(\mathbf{r}_U \mathbf{r}_B^T - \mathbf{r}_B \mathbf{r}_U^T) \mathbf{P}}{a'^2} \end{bmatrix} \quad (25)$$

$$\boldsymbol{\Upsilon}_\tau = \begin{bmatrix} \mathbf{0}_U^T & \frac{\mathbf{P}^T}{c \|\mathbf{P}\|} \end{bmatrix}^T, \quad (26)$$

where $g \triangleq p_y \cos \zeta_0 - p_x \sin \zeta_0$, $\dot{\mathbf{p}}_\theta \triangleq [p_x p_z, p_y p_z, -a^2]^T$, $a \triangleq \sqrt{p_x^2 + p_y^2}$, $a' \triangleq \sqrt{p_x'^2 + p_y'^2}$, $[p'_x, p'_y, p'_z]^T \triangleq \mathbf{R} \mathbf{p}$, and

$$\mathbf{R} \triangleq [\mathbf{r}_1, \mathbf{r}_2, \mathbf{r}_3] = \begin{bmatrix} \cos \zeta_0 & -\sin \zeta_0 \cos \chi_0 & -\sin \zeta_0 \sin \chi_0 \\ \sin \zeta_0 & \cos \zeta_0 \cos \chi_0 & \cos \zeta_0 \sin \chi_0 \\ 0 & -\sin \chi_0 & \cos \chi_0 \end{bmatrix}.$$

Subsequently, for DLP, we can isolate the spatial and temporal parts and write,

$$\mathbf{J}_{\mathbf{o}, \mathbf{p}}^{\text{e}, \text{b}} = \underbrace{\mathbf{\Upsilon}_s \mathbf{J}_{\vartheta\vartheta}^{\text{e}, \text{b}} \mathbf{\Upsilon}_s^T}_{\text{Spatial Part}} + \underbrace{J_{\tau\tau} \mathbf{\Upsilon}_\tau \mathbf{\Upsilon}_\tau^T}_{\text{Temporal Part}}. \quad (27)$$

3) *Performance Comparison of DLP with OWL*: To compare DLP with OWL, recall that for OWL, $\mathbf{J}_{\mathbf{o}, \mathbf{p}}^{\text{e}, \text{b}}$ has the same expression as (27), but with $J_{\tau\tau} = J_{\tau^b}$. Therefore, in comparison with (21), DLP outperforms OWL when

$$J_{\tau^b} < 4(J_{\tau^f}^{-1} + J_{\tau^b}^{-1})^{-1} = J_{\tau^b} \frac{4J_{\tau^f}}{J_{\tau^f} + J_{\tau^b}},$$

which leads to $J_{\tau^f} > \frac{1}{3}J_{\tau^b}$.

This means that, when the bandwidth is equal in both directions, the forward link should have at least one third the SNR of the backward link for DLP to outperform OWL. From Appendix A in [13], it can be seen that this mainly depends on the transmit and receive beamforming.

V. SIMULATION RESULTS AND DISCUSSION

In this section, we numerically investigate and compare the DLP and OWL. Since DLP involves forward and backward transmission, we select equal number of antennas at the BS and the UE to make a fair comparison. Towards that, we consider a BS and a UE both with 12×12 uniform rectangular antenna array communicating via a LOS. Moreover, we assume that the BS array is located in the xz -plane centered about the 3D origin, thus has orientation of $[0^\circ, 0^\circ]^T$. The UE is located in a diamond shape area defined by $(0, 0, -10)$, $(25\sqrt{3}, 25, -10)$, $(0, 50, -10)$, and $(-25\sqrt{3}, 25, -10)$. That is, the BS height is 10 meters. We focus on two cases of orientation: $\mathbf{o} = [0^\circ, 0^\circ]^T$ and $\mathbf{o} = [15^\circ, 15^\circ]^T$. Finally, at a distance d_0 , the channel gain is modeled as

$$\beta = \frac{\lambda}{4\pi d_0} e^{j\frac{2\pi d_0}{\lambda}}, \quad (28)$$

We select $f = 38$ GHz, and $W = 125$ MHz, transmitted power $E_t/T_s = 0$ dBm, $N_0 = -170$ dBm/Hz, and $N_s = 64$ pilot symbols. We further assume an ideal sinc pulse-shaping filter with $W_{\text{eff}}^2 = W^2/3$. Similar to [10], we adopt *fixed* directional beamforming with $N_{\text{bB}} = N_{\text{bU}} = 25$ such that

$$\mathbf{f}_{\text{B}, b} = \frac{1}{\sqrt{N_{\text{bB}}}} \mathbf{a}_{\text{B}}(\theta_{\text{B}, b}^f, \phi_{\text{B}, b}^f),$$

$$\mathbf{w}_{\text{B}, b} = \frac{1}{\sqrt{N_{\text{bB}}}} \mathbf{a}_{\text{B}}(\theta_{\text{B}, b}^w, \phi_{\text{B}, b}^w), \quad 1 \leq b \leq N_{\text{bB}},$$

are BS transmit and receive beams pointing towards $(\theta_{\text{B}, b}^f, \phi_{\text{B}, b}^f)$ and $(\theta_{\text{B}, b}^w, \phi_{\text{B}, b}^w)$, respectively. The transmit and receive beamforming at UE can be similarly defined. The beam directions at the BS are chosen to be equispaced on the sector, while

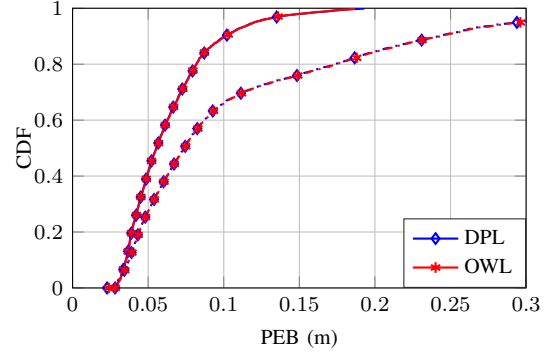


Fig. 3. CDF of PEB with UE orientation angles of 0° (solid) and 15° (dash-dot). $N_U = N_B = 144$, $N_B = 25$.

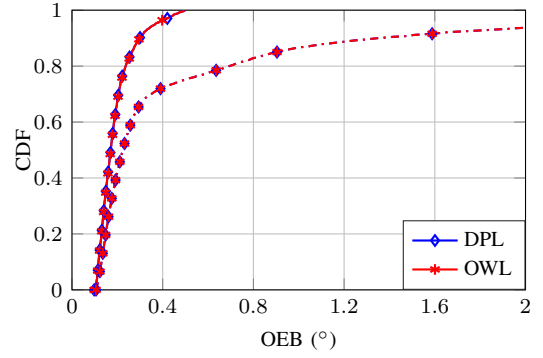


Fig. 4. CDF of OEB with UE orientation angles of 0° (solid) and 15° (dash-dot). $N_U = N_B = 144$, $N_B = 25$.

at the UE, they are reversed to point upwards, rotated with respect to the UE frame of reference by the same orientation angles specified in the studied experiment. Consequently, for $i, j \in \{\text{B}, \text{U}\}$, $i \neq j$, the resulting SNR is

$$\text{SNR} [\text{dB}] = 150.26 + 20 \log_{\text{B}_0} (|\beta| \|\mathbf{a}_i \mathbf{F}_i\| \|\mathbf{a}_j \mathbf{W}_j\|).$$

A. PEB with 0° and 15° UE Orientation

The PEB with zero orientation angles is provided in Fig. 3 (solid lines). It can be seen that DLP provides no improvement over OWL in the considered setup. Despite that, DLP is still a better approach since it alleviates the need of tight synchronization, with the added cost of UE-BS coordination. As discussed in Section IV-3, DLP and OWL have the same spatial component, but DLP has higher temporal information content. However, Fig. 3 shows almost identical results for both protocols, which means that the additional temporal information in DLP is of little importance, and hence the localization performance is limited by the angles estimation rather than the estimation of the time delay. More on this issue will be discussed in Section V-C.

The PEB with $\mathbf{o} = [15^\circ, 15^\circ]^T$ is denoted by the dash-dot lines in Fig. 3. The overall observation from this figure is that the performance worsens as beams steer away, leading to UE mis-orientation with respect to BS. This can result in a loss of beamforming gain that depends non-linearly on the UE location.

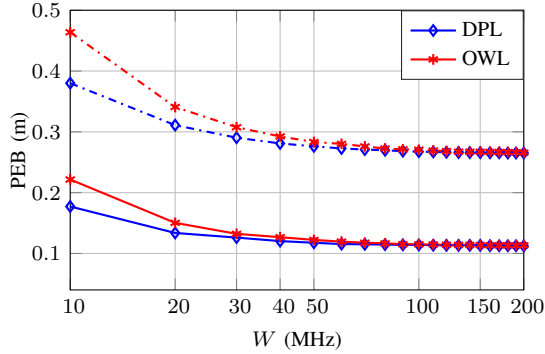


Fig. 5. PEB at 0.9 CDF with respect to the bandwidth W , with UE orientation angles of 0° (solid) and 15° (dash-dot).

B. OEB with 0° and 15° UE Orientation

Considering OEB with 0° and 15° UE orientation in Fig. 4, it can be seen that DLP and OWL exhibit identical performance. Note that OEB depends on DOA and DOD, while the enhancement of DLP over OWL is in the temporal domain. Moreover, in comparison with the case of matched orientation, the system can still provide sub-meter PEB under 15° mis-orientation, while providing significantly higher OEB. This means that orientation estimation is more challenging than position estimation.

C. Impact of the System Bandwidth on PEB

In Section V-A, we concluded that the system is limited by the estimation of the angles rather than the time delay. To investigate this further, we now look closer into the impact of the bandwidth. The results shown in Fig. 5 indicate that as the bandwidth increases, the PEB decreases before reaching a floor at around 100 MHz, which leads to the following observations.

Firstly, at the high bandwidths relevant in mmWave, the temporal information is very high compared to the spatial information, and the performance becomes fixed with W , leading the systems to be spatially-limited. Moreover, under mis-orientation, the accuracy of spatial information degrades, and the improved temporal information does not provide any benefit to the performance achieved at lower bandwidths. Furthermore, at lower bandwidths, the amount of temporal information decreases and becomes comparable to the spatial information. Therefore, the weight of the temporal information in the forward transmission becomes more significant, and the OWL and DLP diverge.

D. Impact of N_B and N_U on PEB

We now study the effect of the number of antennas at BS and UE on the PEB under DLP. Fig. 6 illustrates the effect of N_U and N_B on PEB. Note that the PEB curves with respect to N_U are obtained with a fixed $N_B = 144$, and vice versa. It can be seen from Fig. 6 that a higher N_U generally results in a worse performance. This is because with higher N_U , the UE beams become narrower, which requires more beams to cover the area. Moreover, it can be deduced that a higher N_B

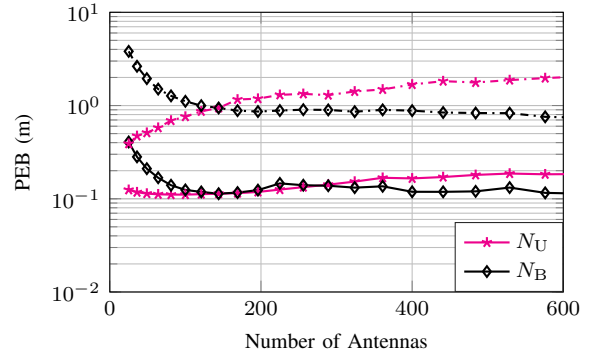


Fig. 6. PEB at 0.9 CDF as a function of N_U and N_B for $N_{b_B} = 25$, with UE orientation angles of 0° (solid) and 15° (dash-dot). PEB curves w.r.t N_U are obtained with $N_B = 144$, while those w.r.t N_B are obtained with $N_U = 144$

will slightly improve the PEB in general. Similar to the case in of N_U , it is understood that the PEB will generally increase when N_B increases, albeit, at N_B values well beyond those displayed in Fig. 6, and with a lesser magnitude than higher N_U . Therefore, adding more antennas at the BS will not reduce the localization performance, as the UE antennas potentially would, at least within the studied range of array size.

Finally, notice that Fig. 6 exhibits some non-monotonic trend. This is due to the nature of directional beamforming, whereby the beamforming gain depends on the user location, number of antennas, and beams directions as detailed in [14].

VI. CONCLUSIONS

Many papers on localization assume that the BS and UE are tightly synchronized. However, usually communication is not synchronized to a high-level useful for localization. Focusing on this issue, in this paper, we considered distributed localization protocol (DLP) and investigated the corresponding PEB and OEB. From the results of the numerical simulation, there was no enhancement observed for DLP over the traditional one-way localization in terms of PEB and OEB. That is, the localization was angle-limited rather than delay-limited. For future work, multipath propagation would be a relevant extension, since scatterers may differ in the uplink and downlink, depending on the beam directions.

ACKNOWLEDGMENT

The authors wish to thank Dr. Xiagyun Zhou of the Australian National University for his valuable feedback.

This work is supported in part by the Australian Government's Research Training Program (RTP), the Horizon2020 projects HIGHTS (High precision positioning for cooperative ITS applications) MG-3.5a-2014-636537 and 5GCAR (Fifth Generation Communication Automotive Research and innovation), the VINNOVA COPPLAR project funded under Strategic Vehicle Research and Innovation Grant No. 2015-04849, and the Spanish Ministry of Economy, Industry and Competitiveness under Grants TEC2017-89925-R and TEC2017-90808-REDT.

APPENDIX

DERIVATION OF THE ELEMENTS OF \mathbf{J}_{φ_D}

From (18), we define

$$\mathbf{J}_{\boldsymbol{\theta}\boldsymbol{\theta}}^b \triangleq \begin{bmatrix} J_{\theta_B\theta_B}^b & J_{\theta_B\phi_B}^b & J_{\theta_B\theta_U}^b & J_{\theta_B\phi_U}^b \\ J_{\theta_B\phi_B}^b & J_{\phi_B\phi_B}^b & J_{\phi_B\theta_U}^b & J_{\phi_B\phi_U}^b \\ J_{\theta_B\theta_U}^b & J_{\phi_B\theta_U}^b & J_{\theta_U\theta_U}^b & J_{\theta_U\phi_U}^b \\ J_{\theta_B\phi_U}^b & J_{\phi_B\phi_U}^b & J_{\theta_U\phi_U}^b & J_{\phi_U\phi_U}^b \end{bmatrix} \quad (29)$$

and

$$(\mathbf{J}_{\boldsymbol{\theta}\beta}^b)^T \triangleq \begin{bmatrix} J_{\theta_B\beta_R}^b & J_{\phi_B\beta_R}^b & J_{\theta_U\beta_R}^b & J_{\phi_U\beta_R}^b \\ J_{\theta_B\beta_I}^b & J_{\phi_B\beta_I}^b & J_{\theta_U\beta_I}^b & J_{\phi_U\beta_I}^b \end{bmatrix} \quad (30)$$

For the case of zero-mean additive correlated Gaussian noise, the FIM of φ_D defined in (16), is given by [15]

$$J_{xy}^b \triangleq \frac{1}{N_0} \int_0^{T_o} \Re \left\{ \frac{\partial \boldsymbol{\mu}^H(t)}{\partial x} (\mathbf{W}_B^H \mathbf{W}_B)^{-1} \frac{\partial \boldsymbol{\mu}(t)}{\partial y} \right\} dt, \quad (31)$$

where $x, y \in \{\theta_B, \phi_B, \theta_U, \phi_U, \beta_R, \beta_I, \tau\}$, and $\boldsymbol{\mu}(t)$ is the mean of the observation vector in (11), and T_o is assumed to be long enough to receive the entire pilot signal. That is,

$$\boldsymbol{\mu}(t) = \sqrt{N_B N_U E_t} \beta \mathbf{W}_B^H \mathbf{a}_B \mathbf{F}_U^H \mathbf{F}_U \mathbf{s}_U(t - \tau^b). \quad (32)$$

Differentiating $\boldsymbol{\mu}(t)$ w.r.t channel parameters and substituting in (31), while defining $\mathbf{P}_A \triangleq \mathbf{A} (\mathbf{A}^H \mathbf{A})^{-1} \mathbf{A}^H$, and $\gamma \triangleq N_B N_U N_s E_t / N_0$, it can be shown that

$$J_{\theta_B\theta_B}^b = \gamma |\beta|^2 \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_U \right) \left(\mathbf{k}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{k}_B \right) \quad (33a)$$

$$J_{\phi_B\phi_B}^b = \gamma |\beta|^2 \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_U \right) \left(\mathbf{p}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{p}_B \right) \quad (33b)$$

$$J_{\theta_B\theta_U}^b = \gamma |\beta|^2 \left(\mathbf{k}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{k}_U \right) \left(\mathbf{a}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right) \quad (33c)$$

$$J_{\phi_U\phi_U}^b = \gamma |\beta|^2 \left(\mathbf{p}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{p}_U \right) \left(\mathbf{a}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right) \quad (33d)$$

$$J_{\beta_R\beta_R}^b = J_{\beta_I\beta_I}^b, \\ = \gamma |\beta|^2 \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_{R2} \right) \left(\mathbf{a}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right), \quad (33e)$$

$$J_{\theta_B\phi_B}^b = \gamma |\beta|^2 \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_U \right) \left(\mathbf{p}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{k}_B \right), \quad (33f)$$

$$J_{\theta_B\theta_U}^b = \gamma |\beta|^2 \left(\mathbf{k}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_U \right) \left(\mathbf{k}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right), \quad (33g)$$

$$J_{\theta_B\phi_U}^b = \gamma |\beta|^2 \left(\mathbf{p}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_U \right) \left(\mathbf{k}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right), \quad (33h)$$

$$J_{\theta_B\beta_R}^b = \gamma \Re \left[\beta^* \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_U \right) \left(\mathbf{k}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right) \right], \quad (33i)$$

$$J_{\theta_B\beta_I}^b = -\gamma \Im \left[\beta^* \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_U \right) \left(\mathbf{k}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right) \right], \quad (33j)$$

$$J_{\phi_B\theta_U}^b = \gamma |\beta|^2 \left(\mathbf{k}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_U \right) \left(\mathbf{p}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right), \quad (33k)$$

$$J_{\phi_B\phi_U}^b = \gamma |\beta|^2 \left(\mathbf{p}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_U \right) \left(\mathbf{p}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right), \quad (33l)$$

$$J_{\phi_B\beta_R}^b = \gamma \Re \left[\beta^* \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_U \right) \left(\mathbf{p}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right) \right], \quad (33m)$$

$$J_{\phi_B\beta_I}^b = -\gamma \Im \left[\beta^* \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{a}_U \right) \left(\mathbf{p}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right) \right], \quad (33n)$$

$$J_{\theta_U\phi_U}^b = \gamma |\beta|^2 \left(\mathbf{p}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{k}_U \right) \left(\mathbf{a}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right), \quad (33o)$$

$$J_{\theta_U\beta_R}^b = \gamma \Re \left[\beta^* \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{k}_U \right) \left(\mathbf{a}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right) \right], \quad (33p)$$

$$J_{\theta_U\beta_I}^b = -\gamma \Im \left[\beta^* \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{k}_U \right) \left(\mathbf{a}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right) \right], \quad (33q)$$

$$J_{\phi_U\beta_R}^b = \gamma \Re \left[\beta^* \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{p}_U \right) \left(\mathbf{a}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right) \right], \quad (33r)$$

$$J_{\phi_U\beta_I}^b = -\gamma \Im \left[\beta^* \left(\mathbf{a}_U^H \mathbf{F}_U \mathbf{F}_U^H \mathbf{p}_U \right) \left(\mathbf{a}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right) \right]. \quad (33s)$$

where $\mathbf{k}_i = \frac{\partial}{\partial \theta_i} \mathbf{a}_i$, $\mathbf{p}_i = \frac{\partial}{\partial \phi_i} \mathbf{a}_i$, such that $i \in \{B, U\}$. To compute $J_{\tau\tau}$, in (21), we extend the results in [10] to

$$J_{\tau^b} = \frac{1}{4\gamma |\beta|^2 \pi^2 W_{\text{eff}}^2 \|\mathbf{a}_U^H \mathbf{F}_U\|^2 \left(\mathbf{a}_B^H \mathbf{P}_{\mathbf{W}_B} \mathbf{a}_B \right)}, \quad (34a)$$

$$J_{\tau^f} = \frac{1}{4\gamma |\beta|^2 \pi^2 W_{\text{eff}}^2 \|\mathbf{a}_B^H \mathbf{F}_B\|^2 \left(\mathbf{a}_U^H \mathbf{P}_{\mathbf{W}_U} \mathbf{a}_U \right)}, \quad (34b)$$

where,

$$W_{\text{eff}}^2 = \int_{-W/2}^{W/2} f^2 |P(f)|^2 df.$$

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